KICZALES, M.

Construction from cast or soldered parts? p. 8. TEHNICA NOUA.

(Asociatia Stiintifica a Inginerilor si Tehnicienilor) Fucuresti.

Vol. 3, No. 40, Mar. 1956.

So. East European Accessions List Vol. 5, No. 9 September, 1956

GOERTZ, Franciszek; KICZKA, Witold

Trials with application of vitamin B_{12} in prevention and therapy of the sequels of toxic diphteria; preliminary communication. Polski tygod.lek. 10 no.21:675-676 23 My '55.

1.(Z Kliniki Chorob Zakasnych Sl. Akad.Med. Wojewodski Sspital Zakazny w Bytomiu; kierownik: sast.prof. dr Francissek Goerts)
Bytom, Wojw.Szpital Zakazny.

(DIPHTERIA

toxoid sequels prev. & ther., vitamin B₁₂.)

(VITAMIN B₁₂, ther. use
diphteria, toxoid, sequels)

KICZKA, Witold; SZPECHT, Jozef

14.

Case of septicemia during angina complicated by stomach rupture. Polski tygod. lek. 14 no.6:258-260 9 Feb 59.

1. (Z Kliniki Chorob Zakaznych Slaskiej Akademii Medycznej w Bytomiu; kierownik kliniki: doc. dr ned. K. Szymonski). Adres: Byrom, Kl. Chor. Zak. Sl. A.M.

(SEPTICEMIA AND BACTERIA, etiol. & pathogen.
septicemia caused by tonsillitis & perforated
peptic ulcer (Pol.)).
(PEPTIC UICER, perf.
with septicemia caused by tonsillitis,
case report (Pol.))
(TONSILLITIS, compl.
septicemia, with perf. of peptic ulcer

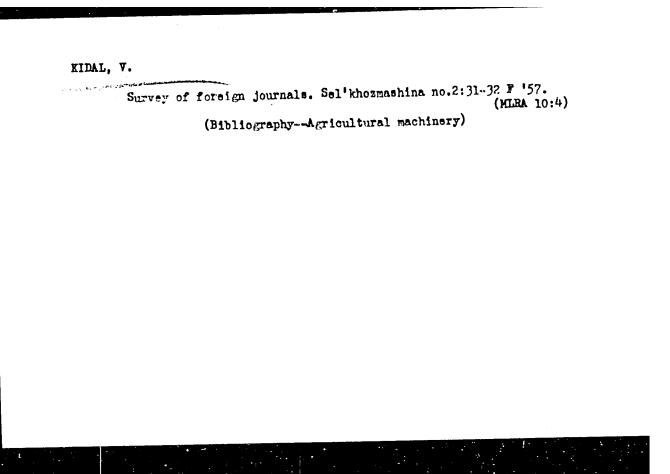
APPROVED FOR RELEASE: 06/13/2000 CIA-RDP86-00513R000722510017-6"

(Pol))

MMICZOK, Frantise, MUDr.; KICZMER, Jan

New trends in popular resuscitation technique. Find givin Cz 12 no.4:206-207 Ap $^{1}62$.

1. Krajsky ustav narodniho zdravi, Ostrava (for Malezok). 2. Elektrarny IX. sjezdu Komunisticke strany Ceskoslovenska, Karvina (for Kiesmer).



KIDAL, V.K.

Items from foreign journals. Trakt. i sel'khozmash. no.4:47 Ap '59.
(NIRA 12:5)
(Agricultural machinery)

DZHAVAKHAYN, T.V., inzh.; KIDALINSKIY, L.P.; KHATSKELEVICH, M.N., inzh.; KLIMOV, N.N., inzh.

Reply to the inquiries of our readers. Elek. i tepl. tiaga 7 no.3:36-37 Mr 163. (MIRA 16:6)

1. Glavnyy inzh. Muromskogo zavoda im. F.E. Dzerzhinskogo (for Kidalinskiy).

(Electric railroads)

TRESKOV, Yu.F., inzh.; KIDALINSKIY, V.L., inzh.

Trubotransformer with a high rated gear ratic. Vest. TSNII MPS 24 no.5:22-26 '65. (MIRA 18:9)

1. Vsesoyuznyy nauchno-issledovatel'skiy teplovoznyy institut.

SMIRNOVA, M.N.; KIDALOV, I.V., student

Some new data on Karpinskii's "initial ridge" belt. Trudy GNI no.21:64-71 '59. (MIRA 14:5) (Russian Platform --Geology, Structural)

LOBODZINSKA, Maria; KIDANKIEWICZ, Tadeusz; SKURSKA, Zofia.

Selective hemagglutination of myxoviruses. Arch. immun. ther. exp. 12 no.2:164-172 '64

1. Department of Virology, Institute of Immunolog and Experimental Therapy, Polish Academy of Sciences, Wroclaw.

MAKOWER, Henryk; SKURSKA, Zofia; LOBODZINSKA, Maria; KIDANKIEWICZ, Tadeusz

Variability of Asian influenza virus cultured in chick embryo allantois. Posteny hig. med. dosw. 12 no.3:291-292 1958.

1. Instytut Immunologii i Terapii Doswindczalnej PAN im. Ludwika Hirszfelda Dział Wirusologii Wrocław, ul. Chalubinskiego 4. (INFLUENZA VIRUSES, culture, Asian strains in chick embryo allantois, variability (Pol))

SKURSKA, Zofia; LOBODZINSKA, Marianna; KIDANKIEWICZ, Tadeusz; BALTOWSKA, Zofia; MAKOWER, Henryk.

Area irrigated with sewage. Its hygienic and sanitary evaluation. VII. Virological studies on sewage and rodents from fields irrigated with sewage water. Acta microbiol. pol. 10 no.4:457-468 '61.

1. Z Zakladu Wirusologii Instytutu Immunologii i Terapii Doswiadczalnej Polskiej Akademii Nauk we Wroclawiu. (SEWAGE virol) (RODENTS virol) (VIRUSES)

SURNAME, Given Names

Country: Poland

Academic Degrees:

Affiliation:

Source: Warsaw, Postepy Higieny 1 Medycyny Doswiadczalnei, Vol XV, No 1
1961, pp 440-441.

Data: "Early and Late Influenza Virus Strains in Tissue Cultures of the Embryo." English abstract of article originally published Arch. Immunol. i Terapii Dosw. 1960, 8, 101.

Authors:

SKURSKA, Z/ofia, PhD, Deputy Chief, Department of Virology (Zak SKURSKA, Z/ofia, PhD, Deputy Chief, Department of Virology and Experimental Therapy (Instytut Immunologii i Terapii Doswiadczalnej mental Therapy, Molekoler, Henryk, MD., M Sc., Chief, Department of Virology, Ludiku Hirszfeld Institute of Immunology and Experimental Therapy, Academy of Sciences, Wroclaw; Director: Prof. Stefan SLOPEK, Syphical Ska, M.

KIDANKIEWICZ, T.

KIDANOVA, Z.S. (Moskva, D-182, N. Bodraya ulitsa, dom 11, kv.13)

Dynamics of the changes in the ballistocardiogram following surgery on the chest cavity in pulmonary tuberculosis.

Grud. khir. 6 no.1:109-111 Ja-F '64. (MIRA 18:11)

KOSITSKIY, G.I.; AGRACHEV, G.I.; VYSOKOVA, T.M.; KALANDADZE, Z.F.; KIDANOVA, Z.S.

Disorders of respiratory and circulatory function in chronic fibrous-cavernous pulmonary tuberculosis and their pathogenesis. Probl. tub. 38 no.3:75-83 '60. (MIRA 14:5)

1. Iz Nauchno-issledovatel'skogo instituta tuberkuleza Ministerstva zdravookhraneniya RSFSR (dir. V.F.Chernyshev, zamestitel' direktora po nauke - prof. D.D.Aseyev).

(TUBERCULOSIS) (RESPIRATORY ORGANS-DISEASES)

(BLOOD-CIRCULATION, DISORDERS OF)

KIDANOVA, Z. S.

Rallistocardiographic observations of pulmonary tuberculosis. Probl. tub. no.2:49-58 '62. (MIRA 15:2)

1. Iz elektrokardiograficheskogo kabineta (zav. - kandidat meditsinskikh nauk G. I. Agrachev) Moskovskogo nauchno-issledovatel¹-skogo instituta tuberkuleza Ministerstva zdravookhraneniya RSFSR (dir. - kandidat meditsinskikh nauk V. F. Chernyshev, zam. dir. po nauchnoy chasti - prof. D. D. Aseyev)

(TUBERCULOSIS) (BALLISTOCARDIOGRAPHY)

AGRACHEV, G.I.; KIDANOVA, Z.S.

Dynamics of electrocardiographic charges following major chest surgery in tuberculosis. Probl.tub. no.6:79-26 161.

(MIRA 14:9)

1. Iz elektrokardiograficheskogo kabineta Moskovskogo nauchnoissledovatel skogo instituta tuberkuleza Ministerstva zdravockhraneniya RSFSR dir. V.F. Chernyshev, zam.dir. po nauchmoy chasti prof. D.D. Aseyev).

(TUBERCULOSIS) (LUNGS--SURGERY)

ROZANOVA, M. D., doktor med. nauk; AGRACHEV, G. I., kand. med. nauk; YYSOKOVA, T. M., kand. med. nauk; KIDANOVA, Z. S.; MIRONOV, F. F.

Effect of exercise therapy on the functional state of adolescents with pulmonary tuberculosis. Probl. tub. 40 no.5:56-63 162.

(MIRA 15:7)

1. Iz Moskovskogo nauchno-issledovatel'skogo instituta tuberkuleza Ministerstva zdravookhraneniya RSFSR (dir. - kandidat meditsinskikh nauk V. F. Chernyshev, zam. dir. po nauchnoy chasti prof. D. D. Aseyev).

(TUBERCULOSIS) (EXERCISE THERAPY)

VYSOKOVA, T.M., kand.med.nauk; AGRACHEV, G.I., kand.med.nauk; KIDANOVA, Z.S.; SOLDATOV, V.Ye., kand.med.nauk

Functional state of respiratory organs and the cardiovascular system in patients with fibrocavernous pulmonary tuberculosis.

Probl. tub. 42 no.3:13-18 '64. (MIRA 18:1)

1. Otdeleniye funktsional'noy diagnostiki i fizicheskikh metodov lecheniya (rukovoditel' S.R.Iachinyan) i 3-ye terapevticheskoye otdeleniye (rukovoditel' - prof. I.E.Sorkin) Moskovskogo nauchno-issledovatel'skogo instituta tuberkuleza (direktor - T.P.Mochalova; zamestitel' direktora po nauchnoy chasti - prof. D.D.Aseyev) Ministerstva zdravookhraneniya RSFSR.

SPAFARIY, Nikolay Milesku (1636-1708); SOLOV'YEV, V.; KIDEL', A.; YUSTRATOVA, N., red.; POLEVAYA, Ye., tekhn. red.

[Siberia and China] Sibir' i Kital. Kishinev, Gos. izd-vo
"Kartia moldoveniaske," 1960. 514 p. (MIRA 14:10)

(Siberia—Description and travel)

(China—Description and travel)

KIDEL', S.S.

informatsii.

[Present-day developments in lighting engineering abroad; survey of foreign technology] Sovremennoe sostoianie svetotekhniki za rubezhom; obzor zarubezhnoi tekhniki (OZT-89). Moskva, TSentr. ir.-t nauchno-tekhn. informatsii elektrotekhn. promyshl. i priborostroeniia, 1962. 59 p. (MIRA 17:9)

1. Moscow. Vsesoyuznyy institut nauchnoy i tekhnicheskoy

KIDER, F.

For further success of our gliders. p. 196. (Kridla Vlasti, No. 7, Apr 1957, Praha, Czechoslovakia)

SO: Monthly List of East European Accessions (EEAL) LC, Vol. 6, No. 8, Aug 1957. Uncl.

LOSTINGS BRY(\$)/BRA(\$)/

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KIDIN, I. N., Engr. Cand. Tech. Sci.

Dissertation: "Effect of High-Frequency Hardening on the Mechanical Properties and Structure of Steel." Moscow Order of the Labor Red Panner Inst of Steel imeni I. V. Stalin, 29 May 47.

SO: Vechernyaya Moskva, May, 1947 (Project #17836)

IA 1/40T70

KIDIN, I. N.

Jun 48

USSR/Metals Steel, Carbon Tempering

"Effect of High Frequency Tempering on the Structure and Strength of Carbon Steel," I. N. Kidin, Cand Tech Sci, Moscow Steel Inst, 5 pp

"Stal" No 6

Great effects of high frequency tempering of carbon steel can be achieved only after close determination of structure and high degree of hardness of steel. Important factors in high frequency tempering are tempering temperature and speed with which various parts are heated by high frequency currents.

KIDIN, I. N.

PA 37/49T98

USSR/Metals

Jun 48

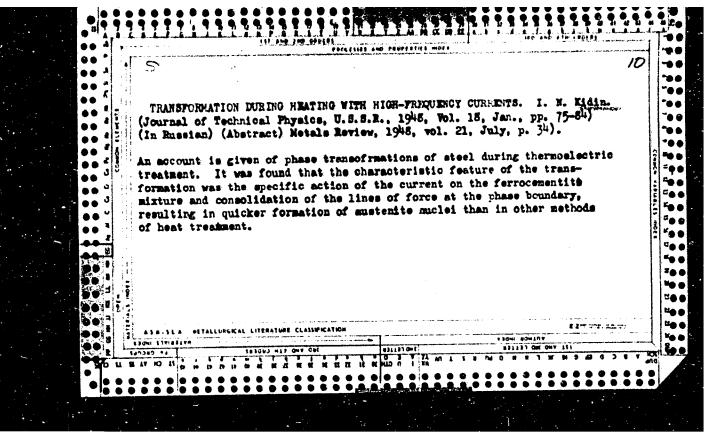
Tool Steel, Tempering

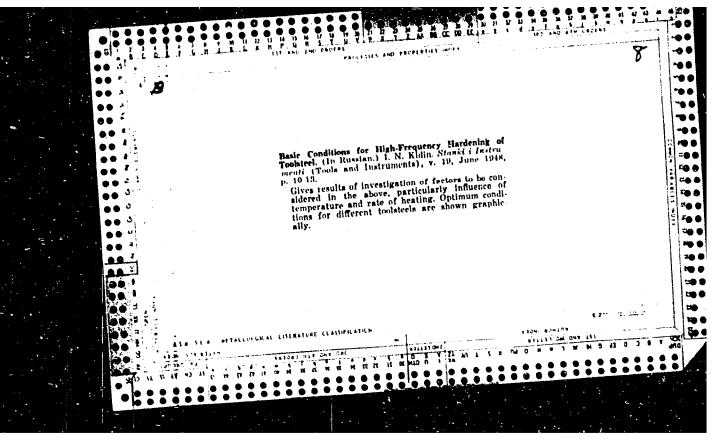
"Fundamental Parameters for High-Grade Tempering of Tool Steel," I. N. Kidin, Cand Tech Sci, Moscow Steel Inst imeni I. V. Stalin, 32 pp

"Stanki i Instrument" No 6

Treats under: method of determining speed of highfrequency tempering, conditions of experiment, effect of tempering temperature on structure and hardness of steel, effect of speed of tempering on structure and hardness of steel, and conclusions.

37/49198





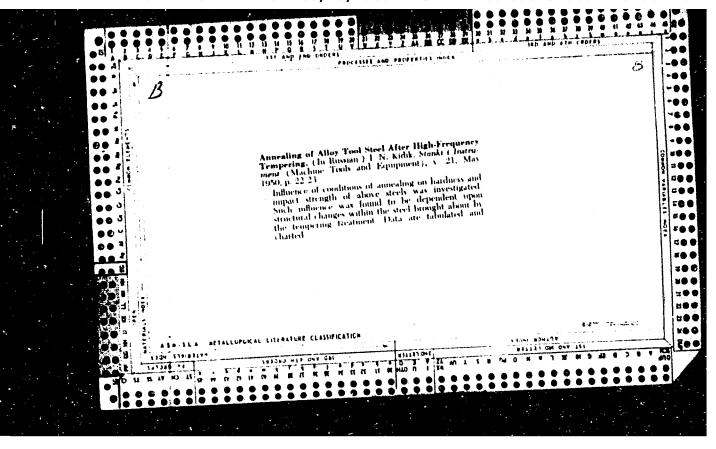
Kilin, T. H. - "The properties of structural steel to perel 1. len inv with him frequency current", Shormik (Mosk. in-t stall in Stalling), 27, 1649, p. 34-50, - Bibliog: 7 Dems.

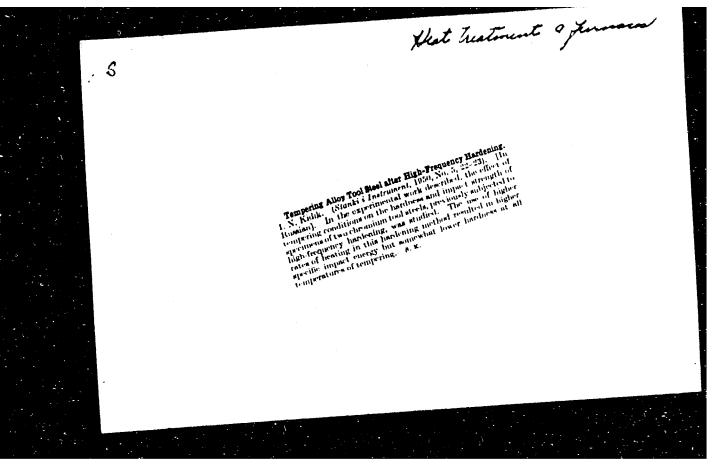
50: U-3042, 11 March 53, (Lotopis 'Zhurnal 'nykh Statey, W. 6, 1040'.

KIDIN, J. N.

Induction Hardening (Termitcheskaia Obrabotka Stali pri Inductsionnom Hagreve), 316 pp, Government Scientific- Technical Publishing House of Ferrous and Non-Ferrous Metallurgy, Moscow, 1950.

Book, B-68125, 1 Sep 53



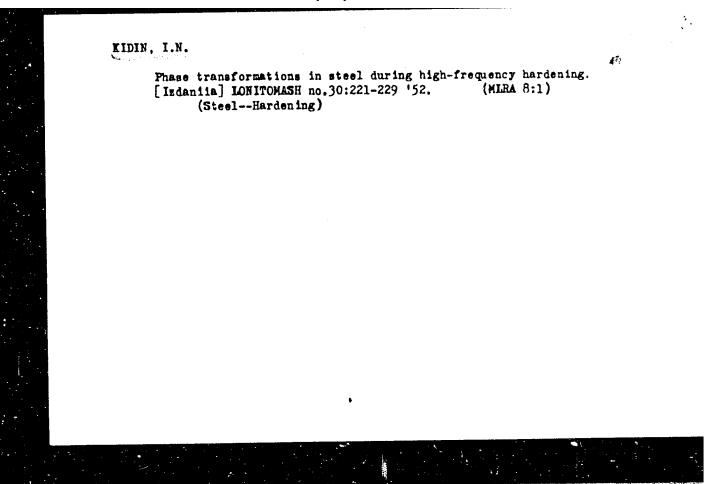


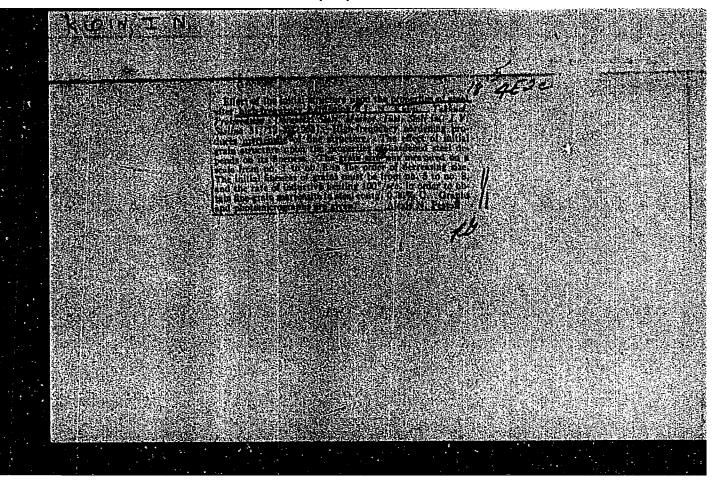
KIDIN, J. N.

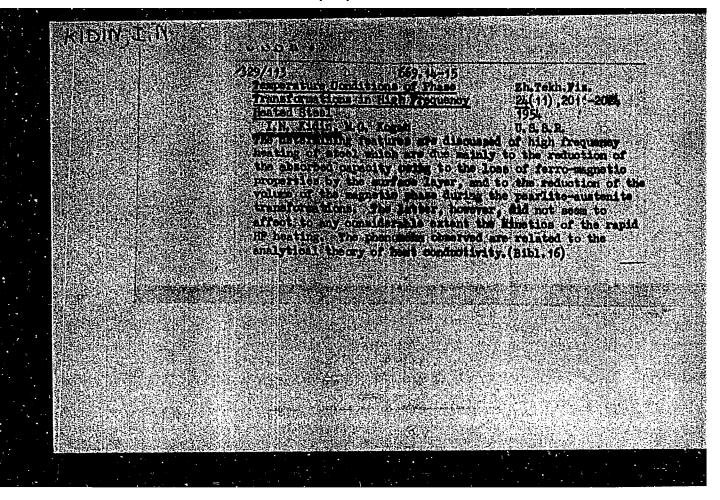
Metals - Heat Treatment

Industion tempering. Nauka i zhizn' 19 No. 6 (1°52)

Monthly List of Russian Accessions, Library of Congress, September 1°52. UNCLASSIFIED.







KIDIN, Ivan Nikolayevich

(Moscow Order of Labor Red Banner Inst of Steel imeni Stalin) - Academic degree of Doctor of Technical Sciences, based on his defense, 19 June 1955, in the Council of the Inst of Metallurgy imeni Baykov of the Acad Sci USSR, of his dissertation entitled: "Phase Transformations in Steel When Heated by Induction," and the academic title of Professor - Chair: "Heat Treatment."

Academic degree and/or title: Doctor of Sciences and Professor

SO: Decisions of VaK, List no. 1, 7 Jan 56, Byulleten' MVO SSSR, Uncl. JPRS/NY-548

KIDIN, I. N.; KRYUKOV, S. N.; ZAKMAROV, E. K.;

"The Examination of the Heterogeneity of Steel by its Carbon Distribution After High-Frequency Hardening," in book The Application of Radioisotopes in Metallurgy, Symposium XXXIV; Moscow; State Publishing House for Literature on Ferrous and Nonferrous Metallurgy, 1955.

I. N. KIDIN, Chair of Metallography and Heat Treatment, Chair of Physical Chemistry, Moseow Inst. of Steel im I. V. Stalin; KRYUKOV, S. N. (Ass't); ZAKMAROV, E. K. (Engr. Chair of Metallography and Heat Treatment.

KIDIN, I. N.

USSR / Phase Conversions in Solids.

E-5

Abs Jour

: Ref Zhur - Fizika, No 4, 1957, No 9285

Author

: Kidin, I.N.

Title

: Certain Features of the Kinetics of Surface Induction

Heating of Steel.

Orig Pub

: Sb. Mosk. in-ta Stali, 1955, 33, 12-68

Abstract

: A detailed analytic and experimental investigation of the kinetics of the induction heating, considered in connection with the features of the non-stationary process of heat conduction, alternating with the establishment of quasi-stationary states. Particular attention is paid to the deformation of the temperature curve of heating, connected with the transition of the heated material from the ferromagnetic into the paramagnetic state in the phase transfor-

mation.

Card

: 1/1

Chair of metallography & seal Treatment

APPROVED FOR RELEASE: 06/13/2000

CIA-RDP86-00513R000722510017-6"

KIDIN. T.N

Category: USSR/Solid State Physics - Phase transformation of solid bodies E-5

Abs Jour: Ref Zhur - Fizika, No 1, 1957, No 1178

Author : Kidin, I.N.

Title : Basic Stages in the Kinetics of the Formation of Austenite in Induction

Heating

Orig Pub : Sb. Mosk. in-ta stali, 1955, 33, 69-74

Abstract : Three basic types of kinetics of induction heating of steel are established.

In the first case the metal temperature vs. time curves comprise an initial steep straight-line section, a section with variable curvature; and a third less-steep straight-line section. In the second case, the curve consists of a sloping straight line, a straight-line section parallel to the time axis, and again of a sloping straight line. The third type of curve consists of two inclined straight lines. This behavior of the induction-heating curve is due to the redistribution of the heat power delivered during the magnetic transformations, and not by the presence of phase transformations or by the nature

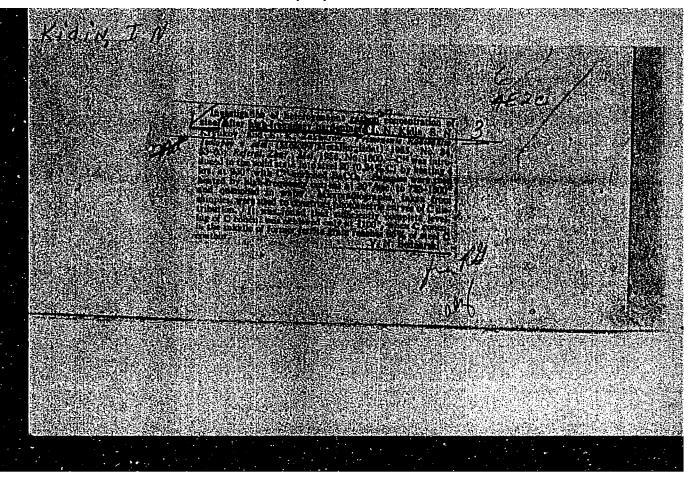
of their development.

Card : 1/1

ZHUKHOVITSKIY, A.A., professor, dekter khimicheskikh mauk; KIDIH, I.H., kandidat tekhnicheskikh mauk, detsent; TRUBIH, K.G., professor, dekter.

Preface. Sber.Inst.stali 34:5-6 '55. (MIRA 9:7) (Physical metallurgy) (Radieactive tracers--Industrial applications)

"APPROVED FOR RELEASE: 06/13/2000 CIA-RDP86-00513R000722510017-6



AL'TGAUZEN, O.N., kandidat fiziko-matematicheskikh nauk; BERNSHTEYN, M.L., kandidat tekhnicheskikh nauk; BLANTER, M.Ye., doktor tekhnicheskikh nauk; BOXSHTEYN, S.Z., doktor tekhnicheskikh nauk; BOLKHOVITINOVA, Ye.N., kandidat tekhnicheskikh nauk; BORZDYKA, A.M., doktor tekhnicheskikh nauk; BUNIN, K.P., doktor tekhnicheskikh nauk; VINOGRAD, M.I., kandidat tekhnicheskikh nauk; VOLOVIK, B.Ye., doktor tekhnicheskikh nauk [deceased]; GAMOV, M.I., inzhener; GELLER, Yu.A., doktor tekhnicheskikh nauk; GORELIK, S.S., kandidat tekhnicheskikh nauk; GOL'DENBERG, A.A., kandidat tekhnicheskikh nauk; GOTLIB, L.I., kandidat tekhnicheskikh nauk; GRIGOROVICH, V.K., kandidat tekhnicheskikh nauk; GULYAYEV, B.B., doktor tekhnicheskikh nauk; DOVGALEVSKIY, Ya.M. kandidat tekhnicheskikh nauk; DUDOVTSEV, P.A., kandidat tekhnicheskikh nauk; KIDIN, I.N., doktor tekhnicheskikh nauk; KIPNIS, S.Kh., inzhener; KORITSKIY, V.G., kandidat tekhnicheskikh mauk; LANDA, A.F., doktor tekhnicheskikh nauk; LEYKIN, I.M., kandidat tekhnicheskikh nauk; LIVSHITS, L.S., kandidat tekhnicheskikh nauk; L'VOV, M.A., kandidat tekhnicheskikh nauk: MALYSHEV.K.A., kandidat tekhnicheskikh nauk; MEYERSON, G.A., doktor tekhnicheskikh nauk; MINKEVICH, A.N., kandidat tekhnicheskikh nauk; MOROZ, L.S., doktor tekhnicheskikh nauk; NATANSON, A.K., kandidat tekhnicheskikh nauk; NAKHIMOV, A.M., inzhener; NAKHIMOV, D.M., kandidat tekhnicheskikh nauk; POGODIN-ALEKSEYEV, G.I., doktor tekhnicheskikh nauk; POPOVA, N.M., kandidat tekhnicheskikh nauk; POPOV, A.A., kandidat tekhnicheskikh nauk; RAKHSHTADT, A.G., kandidat tekhnicheskikh nauk; ROGEL'BERG, I.L., kandidat tekhnicheskikh nauk;

(Continued on next card)

AL'TGAUZEN, O.N. --- (continued) Card 2.

SADOVSKIY, V.D., doktor tekhnicheskikh nauk; SALTYKOV, S.A., inzhener; SOBOLEV, N.D., kandidat tekhnicheskikh nauk; SOLODIKHIN, A.G., kandidat tekhnicheskikh nauk; UMANSKIY, Ya.S., kandidat tekhnicheskikh nauk; UTEVSKIY, L.M., kandidat tekhnicheskikh nauk; FRIDMAN, Ya.B., doktor tekhnicheskikh nauk; KHRUSHCHEV, M.M., doktor tekhnicheskikh nauk; KHRUSHCHEV, M.M., doktor tekhnicheskikh nauk; SHAPIRO, M.M., inzhener; SHKOL'NIK, L.M., kandidat tekhnicheskikh nauk; SHAPIRO, M.M., inzhener; SHKOL'NIK, L.M., kandidat tekhnicheskikh nauk; SHRAYBKR, D.S., kandidat tekhnicheskikh nauk; SHCHAPOV, N.P., doktor tekhnicheskikh nauk; GUDTSOV, N.T., akademik, redaktor; GORODIN, A.M. redaktor izdatel'stva; VAYNSHTEYN, Ye.B., tekhnicheskiy redaktor

[Physical metallurgy and the heat treatment of steel and iron; a reference book] Metallovedenie i termicheskaia obrabotka stali i chuguna; spravochnik. Pod red. N.T.Dudtsova, M.L.Bernshteina, A.G. Rakhshtadta. Moskva, Gos. nauchno-tekhn. izd-vo lit-ry po chernoi i tsvetnoi metallurgii, 1956. 1204 p. (MLRA 9:9)

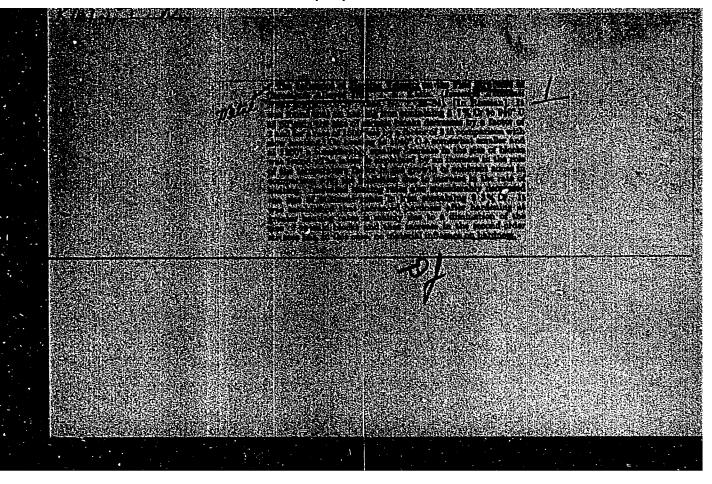
1. Chlen -korrespondent Akademii nauk USSR (for Bunin)
(Steel--Heat treatment)
(Physical metallurgy)

KIDIN, I.N., doktor tekhnicheskikh mauk, professor.

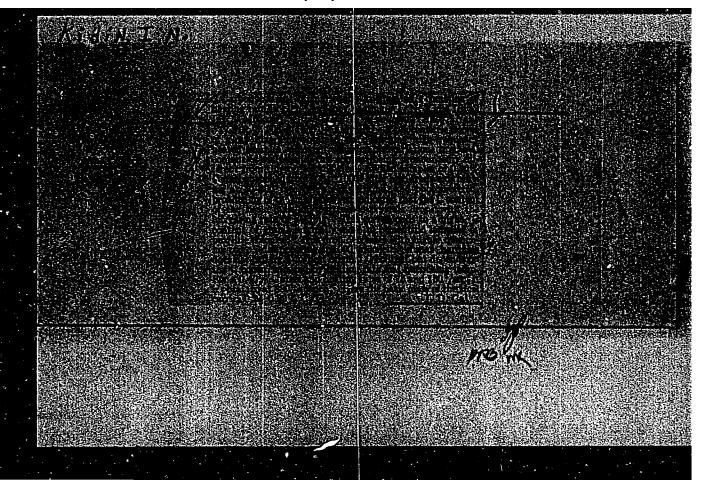
Correlation between induction heating parameters and the grain size of austenite in carbon steel. Metalloved. i obr.met. no.1: 40-41 Ja '56. (MIRA 9:6)

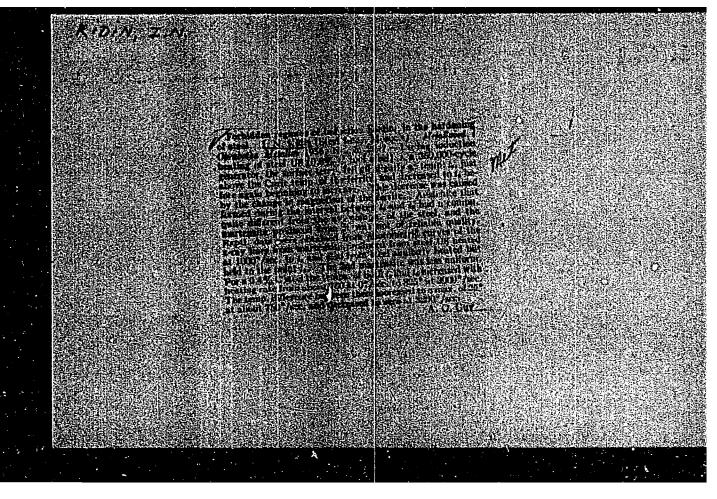
1.Moskovskiy institut stali imeni Stalina. (Steel--Metallography) (Austemite)

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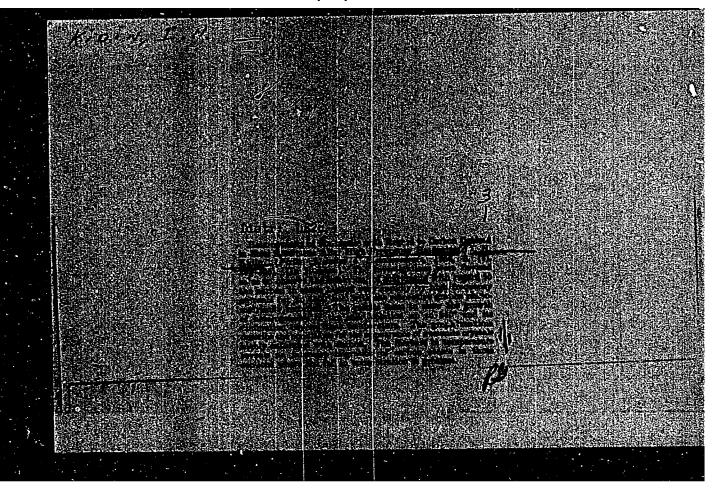


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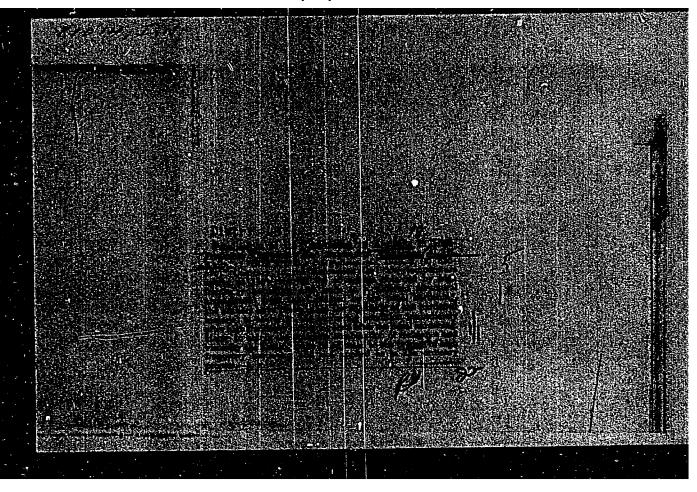




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"APPROVED FOR RELEASE: 06/13/2000 CIA-RDP86-00513R000722510017-6



KIDIN, I.N.

Category: USSR/Solid State Physics - Phase Transformation in Solid Bodies

Abs Jour : Ref Zhur - Fizika, No 2, 1957 No 3826

: Kidin, I.N. Author

: Moscow Institute of Steel, USSR

Inst : Mechanism of Formation of Austenite in Rapid Heating Title

Orig Pub : Dokl. AN SSSR, 1956, 106, No 6, 1019-1022

Abstract : A new mechanism is proposed for the formation and growth of austenite

nuclei. The author proposes that the amount of carbon on the boundaries of the blocks of the mosaic structure of of-iron exceeds its solubility in the -iron. Experiments have shown, that this supersaturation may reach 0.25% and in this case the phase transformation occurs upon rapid heating at 8200. In the case of diffusion migration of the austeniteferrite boundary, there is formed in addition to the diffusion boundary also a boundary complex of minute nuclei. The development of this process leads to the formation of a very finely ground austenite. One should observe simultaneously an increase in the microhardness of the center of the ferrite grain. Experimental measurements were made of the microhardness

: 1/2 Card

APPROVED FOR RELEASE: 06/13/2000 CIA-RDP86-00513R000722510017-6"

Category: USSR/Solid State Physics - Phase Transformation in Solid Bodies

Abs Jour: Ref Zhur - Fizika, No 2, 1957 No 3826

of the grains and the contact electric heating of technically pure iron was investigated with simultaneous oscillographic recording of the thermal and dilatometric curve. Dilatrometric investigations were carried out with Panov's capacitive dilatometer. The measurement results confirmed the predicted theoretical hypotheses.

Card : 2/2 KIDIN, I. N.

"Austenite Formation During Heat Treatment,"

paper presented at the Metallurgical Congress in Chicago, 6 November 1957.

Moscow Steel Inst.

Eval. and Abst. B-3,095,520

KIDIN, IVAN NIKDIAYEVICH

KIDIN Ivan Wikeleyawich, LOZINSKIY, M.G., redaktor; ROZENTSVEYG, Ya.D., redaktor izdatel'stva; MIKHAYLOVA, V.V., tekhnicheskiy redaktor

[Phase conversions during accelerated annealing of steel] Fazovy prevrashchenia pri uskorennom nagreve stali. Moskva, Gos.nauchnotekhn.izd-vo lit-ry po chernoi i tsvetnoi metallurgii, 1957. 92 p. (Steel--Heat treatment) (MIRA 10:9)

SOV/137-59-1-1823

Translation from: Referativnyy zhurnal: Metallurgiva, 1959, Nr 1, p 241 (USSR)

AUTHORS: Kidin, I. N., Bashnin, Yu. A.

TITLE: Certain Specific Technological Properties of High-frequency Harden-

ing Associated With the Kinetics of Induction Heating (Nekotoryye tekhnologicheskiye osobennosti vysokochastotnov zakalki, svyazannyye

s kinetikoy induktsionnogo nagreva;

PERIODICAL: V sb : Prom primenentye tokov vysokov chastoty. Riga, 1957,

pp 123-133

ABSTRACT: A report on the general aspects of the kinetics of induction heating

(IH) and practical recommendations on procedures for high-frequency hardening (HH) are given. Upon attaining $t_{\rm C}$ during IH an inflection point appears on the heating curve which is caused by the decrease and redistribution of the specific power. The basic types of IH kinetics are: Curves with a dip (saddle), a flat top, or an inflection. The phase transformations (PT) proceed in three stages: Nonisothermal in the $A_1 \rightarrow t_{\rm C}$ range, isothermal at $t_{\rm C}$, and nonisothermal at $> t_{\rm C}$. In the case of an inflection the isothermal stage is

Card 1/2 absent. The effect of alloying of steel with Cr. W, and N: on the

Certain Specific Technological Properties of High-frequency Hardening (cont.) SOV/137-59-1-1823

results of HII is examined. The hypothesis on the displacement of PT into the area of more elevated temperatures during IH and the necessity of using higher temperatures during HH than during the usual heating procedure is confirmed. A new thermal parameter of the rate of IH in the PT range (above the inflection point on the curve) is proposed. For a group of steels with 1% Cr and 0.42-1.01%C diagrams are adduced of the prevailing and permissible IH specifications in the coordinates HH temperature vs. IH rate in the PT region. With an increase in the concentration of C there is an expansion of the temperature range of HH which causes increased hardness. An increase in the IH rate widens the zone of prevailing heating. IH is impractical with an IH rate < 50°C/sec. The largest zone of predominant HH performance is observed with IH rates of 200°C/sec.

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Card 2/2

APPROVED FOR RELEASE: PARSE 3/ 2000 EXFIRM PARSO-00513R000722510017-6"

AUTHOR:

See table of contents

TITLE:

Working of Steel and Alloys (Obrabotka stali i splavov)

PUB. DATA:

Gosudarstvennoye nauchno-tekhnicheskoye izdatel'stvo literatury po chernoy i tsvetnoy metallurgii, Moscow

1957, 451 pp., 3,000 copies

ORIG. AGENCY:

Moskovskiy ordena trudovogo krasnogo znameni institut

stali imeni I. V. Stalina

EDITORS:

Responsible Ed.: Kidin, I. N.; Ed. of Publishing House: Dokukina, Ye. V.; Tech. Ed.: Attopovich, M. K. Editorial Council of the Moscow Steel Institute

(Institute stali): Glinkov, M. A., Professor, Doctor; Grigorash, R. N., docent, candidate of tech. sciences; Gudtsov, N. T., Academician (deceased); Yelyutin, V. P., professor, doctor; Zhukhovitskiy, A. A., professor,

doctor; Kidin, I. N., professor, doctor; Livshits, B.G., professor, doctor; Lyubimov, A. P., professor, doctor;

Card 1/15

Pavlov, I. M., corresponding number of the Academy of

working of Steel and Alloys

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TABLE OF

CONTENTS: Gudtsov, N. T., (Deceased), Panchenko, I. P. Titanium-tungsten Alloys

,

It is shown that the microstructural hardness and durability of titanium-tungsten alloys increases with the amount of tungsten in the alloy. There are 2 Soviet references, 1 in English.

Gudtsov, N. T. (Deceased), Chadek, I. The Effect of Alloying Elements on Eutectoid Changes in Steel

The author investigates the effects of structure and chemical composition of the active crystal nucleus in eutectoid changes of steel alloys. The carbide phase in the eutectoid change and in tempering was chosen as a specific example. There are 2 Soviet references, 2 English, 1 Scandinavian.

Kidin, I. N. Kinetics of Induction Heating of Steel Alloys 33
Card 3/15

Working of Steel Alloys

179

Practical experiments carried out by the author with various APPROVEDIFOR RELEASE: 06/13/2000ly sold-thops: -00513R000721510017-6" theory of kinetics in this kind of heating. There are 27 Soviet references.

Kidin, I. N. Formation of Austenite During Induction Heating of Steel Alloys

59

The author arrives at the following conclusions: 1. the hardening temperature of chrome steel should be higher than that of tungsten and molybdenum steels, and 2. the different nature of the kinetics of heating of chrome and nickel steels indicate that with the increase of Cr content the size of the austenite grains decrease and will increase in size with the amount of Ni. There are 3 Soviet references.

Kidin, I. N. High-frequency Hardening of Molybdenum Steel 65

This paper deals with the effect of induction heating parameters on the size of austenite grains of molybdenum steels and on the hardness of this steel after hardening. The conclusion Card 4/15

SOV/137-58-11-23456

Translation from: Referativnyy zhurnal. Metallurgiya, 1958, Nr 11, p 231 (USSR)

AUTHORS: Kidin, I. N., Astafyeva, Ye. V.

TITLE: A Radiographic Investigation of Nonuniformity of Martensite Produced

During Hardening of Steel With Induction Heating (Issledovaniye neo-dnorodnosti martensita, poluchennogo pri zakalke stali s induktsionnym

nagrevom, metodom radiografii)

PERIODICAL: V sb.: Prom. primeneniye tokov vysokov chastoty. Riga, 1957,

pp 194-205

ABSTRACT: Autoradiography methods were employed in an investigation of the

distribution of C in the structure of induction-hardened steel St 20. The C 14 isotope was introduced into the specimens by means of annealing them in vacuum, at a temperature of $1100^{\rm o}$ C for a period of four hours, together with BaCO3 enriched with C 14 . After annealing, the average size of a pearlitic region amounted to approximately $65\,\mu$ and that of a ferritic field to $115\,\mu$. Heating rates (HR) of 30, 130, and 230 degrees/second were employed in the region of phase transform-

ations. At all HR the quenching was performed at temperatures range

Card 1/2 ing from 800 to 1300°. Photometric evaluation of the radiograms

SOV/137-58-11-23456 A Radiographic Investigation of Nonuniformity of Martensite Produced During (cont.)

revealed that the nonuniformity of C distribution at all quenching temperatures in creases with increasing HR. A fully hardened structure may be obtained only at a temperature of 1100° or above. During quenching from a temperature of 900° the concentration of C in the central portions of the formerly pearlitic regions amounts to 0.57°/o at an HR of 30°/sec and 0.75°/o at an HR of 130°/sec. Almost complete equalization of the C concentration was attained only after quenching from a temperature of 1300° at a minimal HR of 30°/sec; at an HR of 230°/sec, the C concentration in the central portions of the formerly pearlitic regions amounted to 0.58°/o and in the ferritic interstices to 0.07°/o only. Regardless of the HR the intensity of diffusion processes is greater at 800-1100° than it is at 1100-1300° owing to a reduction in the gradient of C concentration at temperatures ranging from 1100 to 1300°.

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CIA-RDP86-00513R000722510017-6 "APPROVED FOR RELEASE: 06/13/2000

129-2-3/10

Kidin, I.N., Dr. of Technical Sciences Prof. (Moscow) AUTHOR:

The Kinetics of Dissolution of Carbides in Tungsten Steel During TITLE: Induction Heating. (Kinetika rastvoreniya karbidov vol'framovoy

stali pri induktsionnom nagreve.)

Metallovedeniye i obradotka metallov, 1957, No. 2, pp. 18-23 PERIODICAL:

(U.S.S.R.)

The author investigated processes occurring in tungsten steels ABSTRACT:

and particularly the dissolution of carbides in such steels during high frequency induction heating. The experiments were carried out on alloys containing 1.5 and 10% W and about 0.6 and 1% C; the exact composition of the six tested materials and their Acl and Ac3 points are given in Table 1, p. 19. Prior to high frequency hardening a carbide deposit was separated electrolytically, and after washing and drying was subjected to X-ray analysis using iron radiation. The precipitation was induced with a current density of A/cm2 for fifteen minutes and during

this time an 0.5 to 0.7 mm layer dissolved from the surfact.

It was found that the temperature of intensive dissolution

Card 1/4

129-2-3/10 APPROVED FOR RELEASE: 06/13/2000 CIA-RDP86-00513R000722510017-6" TITLE:

The Kinetics of Dissolution of Carbides in Tungsten Steel During Induction Heating. (Kinetika rastvoreniya karbidov vol'framovoy stali pri induktsionnom nagreve.)

of carbide FegWgC during induction heating is lower than during ordinary heating. In steel containing 0.6% C the tungsten carbide dissolved fully or almost fully at 880°C, if the heating rate was 40°C/sec. By raising the heating rate to 75 C/sec the dissolution of the carbides in the steel containing 1% W is mainly completed at 960°C and in the steel containing 5% W at 1040°C. In the case of a high heating rate (200°C/sec.) an increase in the temperature will be more effective the lower the W content of the steel with 1% C. In steel containing 10% W the dimensions of the particles decrease by 18% at 980 - 1040°C and the corresponding figures are 40% for 5% W and 49% for steel with 1% W as compared to the initial state. With an increasing heating rate the temperature of complete dissolution of the carbides in tungsten steel increases. Stabilisation of the temperature of dissolution of iron-tungsten carbides with increasing heating rate was not observed during the tests. In specimens containing

Card 2/4

129-2-3/10

TITLE:

The Kinetics of Dissolution of Carbides in Tungsten Steel during Induction Heating. (Kinetika rastvoreniya karbidov vol'framovoy stali pri induktsionnom nagreve.)

reduction of the carbide particles can be observed with increasing hardening temperature and decreasing rate of heating to an equal temperature. Table 2 gives data on statistical investigations which shows the chemical composition, the heating temperature, the average partical diameter at various heating speeds and the number of particles per mm at various heating speeds.

The text includes 2 tables and 3 sets of photographs. There are no references.

ASSOCIATION: Moscow Steel Institute (Moskovskiy Institut Stali)

PRESENTED BY: ---

SUBMITTED:

TED: ---

AVAILABLE:

Library of Congress

Card 4/4

CIA-RDP86-00513R000722510017-6 "APPROVED FOR RELEASE: 06/13/2000

AUTHOR:

Kidin, I.N. (Moscow).

24-4-9/34

TITLE:

Investigation of the fine structure of chromium iron tempered after hardening from a high temperature at a high speed. (Issledovaniye tonkoy struktury khromistogo zheleza, otpushchennogo posle zakalki pri nagreve s

bol'shoy skorost'yu).

PERIODICAL:

"Izv. Ak. Nauk, Otd. Tekh. Nauk" (Bulletin of the Ac. Sc., Technical Sciences Section), 1957, No.4, pp.63-69 (USSR).

ABSTRACT:

In earlier published work (8) and (9) the author established that the fine structure of alloyed iron can change not only as a result of volume changes due to phase hardening during cooling but also as a result of formation of the Y-phase during heating of the alloy. These data provide additional experimental confirmation of the hypothesis on the formation of austenite nuclei along the boundaries of coherent regions which increase considerably in quantity and decrease in size owing to the inhibited growth at very high heating rates. To elucidate the differences between the changes in the fine structure and the softening occurring in the case of hardening with high heating rates from those occurring during current type hardening, the authors investigated the fine structure during tempering of iron containing 5.2% Cr after hardening following slow heating and after high frequency hardening with heating rates of 50 and 1000 C/sec during

Card 1/3

Investigation of the fine structure of chromium iron tem-APPROVED FOR TRELEASET 06/13/2000 TOMCIA TREPSE 00/515/7000/525/10617-6" speed. (Cont.) speed. (Cont.)

the second stage. The melt was produced from Armco iron and metallic chromium in a 10 kg induction furnace. After homogenisation annealing, rods of 18 mm dia. were produced by forging; the shaping and dimensions of the specimens were described in an earlier paper (9). The decrease in size of the coherent regions and the increase of Type II stresses during the hardening are determined by three factors: phase hardening caused by volume changes during γ to α -transformation, the intensity of these volume changes which depends on the cooling rate during hardening and the character of the fine structure of the Y-phase which is determined by the inter-relation between the temperature and the heating speed. Comparison of the influence of the fine structure of the austenite and the intensity of γ to α -transformations indicates that the second of these factors is less important. The more metastable the structure which forms after hardening the lower will be the tempering temperature at which an appreciable growth of the coherent zones and a reduction of the Type II stresses begins. The temperature at which a decrease of Type II stresses begins is 200 to 150 C lower than the temperature at which an increase in the dimensions of the

Card 2/3

AUTHOR: Kidin, I.N., Doctor of Technical Sciences, Prof. 129-9-9/14
TITLE: Influence of the parameters of induction heating on the size of the austenitic grain in nickel steel. (Vliyaniye parametrov induktsionnogo nagreva na velichinu zeren austenita nikelevoy stali).

PERIODICAL: "Metallovedeniye i Obrabotka Metallov" (Metallurgy and Metal Treatment), 1957, No.9, pp.36-42 (U.S.S.R.)

ABSTRACT: The conditions of formation of austenite and of its kinetic characteristics during induction heating depends to a certain extent on the mutual position of three temperatures, namely, the beginning of formation of austenite, A1, the Curie point and the temperature of heating during hardening; the first two temperatures are determined by the composition of the steel, the third is chosen not only as a function of the composition of the steel but also as a function of the speed and shape of the induction hardening curve. It is shown that in more highly alloyed steels the influence of the first (pre-isothermal) and second (isothermal) stages of induction heating is

Card 1/4 smaller than in less alloyed steels; the third stage of heating, that following the isothermal stage, is of greatest importance, the temperature range of this stage decreases

CIA-RDP86-00513R000722510017-6" APPROVED FOR RELEASE: 06/13/2000

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CIA-RDP86-00513R000722510017-6"

Influence of the parameters of induction heating on the size of the austenitic grains in nickel steel. (Cont.) with increasing chromium content and increases with increasing nickel content. In this paper the results are described of experimental investigations of nickel steels obtained from about twenty melts, the compositions of which are given in Table 1, p.38. The steel was smelted in a 10 kg capacity induction furnace and, after forging of the ingots into rods and annealing, specimens were produced, the shape of which is shown in Fig.4, p.38. After hardening, the specimens were subjected to a special etching process which permits clear observation of the grain boundaries and, following that, the specimens were viewed by microscope and the grain dimensions determined according to the histogram method. The microphotos, Fig.5, show the change in the grain size of austenite in a steel containing 0.6% C and 1% Ni as a result of increasing the heating temperature at a constant heating rate. The graphs, Fig.6, show the influence of the induction heating parameters on the hardness and grain size of the austenite of nickel steel containing 0.99 to 9.52% Ni. The graphs, Fig.7, show the influence of the temperature, the speed of the induction heating and the nickel content on the austenite grain size in nickel steel containing 0.2, 0.6 and 1% C. Table 2

Card 2/4

Influence of the parameters of induction heating on the size of the austenitic grains in nickel steel. (Cont.) gives the average grain size of the austenite for steels containing 1, 2.5, 5 and 10% Ni and 0.2, 0.4, 0.6, 0.8 and 1% C for hardening temperatures of 800, 880, 960 and 1040 C and heating rates of 40, 50, 75, 130 and 200 C/sec. In all the studied cases the influence of the induction heating parameters on the austenite grain size remained the same; if the heating rate remains unchanged the grain size will increase with increasing temperature. For an equal final heating temperature the grain dimensions of the austenite will decrease with increasing heating speed. Under equal induction heating conditions the austenite grains of nickel steel will grow faster than those of chromium steels of similar composition. One of the main reasons for this is the difference in the position of the critical point A_1 ; of this value by the nickel the owing to lowering transformation temperature range for an equal heating temperature is considerably wider than for chromium steel. Of great importance also is the absence in nickel steel of carbides with difficult solubility, whilst chromium steels do contain such carbides. The three-dimensional diagrams of Fig.7, in which the dependence of the austenite grain

Card 3/4

Kidin, In.

AUTHORS:

Kidin, I. N., and Panov, A. V.

TITLE:

Use of the Capacity Dilatometer for Research of Phase Conversion during Rapid Heating (Primeneniye emkostnogo dilatometra dlya issledovaniya fazovykh prevrashcheniy

pri bystrom nagreve)

PERIODICAL:

Zavodskaya Laboratoriya, 1957, Vol. 23, No. 1, pp. 48-52 (U.S.S.R.)

ABSTRACT:

The authors find that joint thermic and dilatometric analysis generally cannot be used because of the considerable lack of correspondence between the degree of inertness of existing dilatometers and the rapid speed of heating. The oscillcoraph is therefore preferred for recording the temperature curve. In order to record the temperature curve, the authors assembled a special device which enabled them to record changes in the line of heating with a speed of 1 to 10,000 deg/sec. The equipment by which this is done is explained with drawings and graphs: stand for holding the specimen, circuit of the generating unit, circuit of the amplifier for the dilatometer, circuit of the amplifier of the DC to the dilatometer. Thermic and dilatometric curves for technically pure iron with .02% C and .07% C.

Card 1/2

KIDIM I No

137-58-3-5845

Translation from: Referativnyy zhurnal, Metallurgiya, 1958, Nr 3, p 196 (USSR)

AUTHOR:

Kidin, I. N.

TITLE:

Kinetics of Induction Heating of Alloyed Steel (Kinetika

induktsionnogo nagreva legirovannoy stali)

PERIODICAL:

Sb. Mosk. in-t stali, 1957, Vol 36, pp 33-58

ABSTRACT:

The kinetics of induction heating was investigated on a number of specimens of various steels alloyed with Cr, W, Ni, and Mo melted in a 10-kg induction furnace. The content of Cr, W, and Ni amounted to 1.2, 5.5, and 10 percent, while Mo was introduced in amounts equivalent to 0.2, 0.5, 1, and 2 percent. The C content in each alloy was varied in 0.2 percent steps from 0.2 percent to 1 percent. The heating curves were recorded by means of an oscillograph, while the heating process itself was controlled by a photoelectric pyrometer. The experimental data obtained verify the magnetic theory of the kinetics of induction heating, thus making it possible to explain the cause for the considerable changes in heating rates occurring after the completion of phase and magnetic transformations; this explanation is based on the relationship existing between the electromagnetic and temperature

Card 1/2

Chair of Metallography . Heat Treatment of steel

137-58-3-5845

Kinetics of Induction Heating of Alloyed Steel

fields in the inductor-heated object system and the field of physical parameters within the specimen being heated. Bibliography: 27 references.

V.R.

Card 2/2

KIDIN, IN

137-58-3-5846

Translation from: Referativnyy zhurnal, Metallurgiya, 1958, Nr 3, p 196 (USSR)

AUTHOR: Kidin, I. N.

Conditions for the Formation of Austenite During Induction TITLE:

Heating of Alloyed Steel (Usloviya obrazovaniya austenita pri

induktsionnom nagreve legirovannoy stali)

Sb. Mosk, in-t stali, 1957, Vol 36, pp 59-64 PERIODICAL:

Peculiarities of austenite formation, attributable to variations ABSTRACT:

in the kinetics of the heating process as a function of various alloying elements employed, are examined in the process of induction heating of alloyed steel and are compared with those of carbon steel. When the isothermal stage of austenite formation is considerably higher than the A1 temperature and when the temperature difference between the Curie point, t_c, and A_l is comparatively great, then the relative volume in which the first stage (A1 to tc) of the transformation takes place will be greater than it would have been, had the isothermal stage of the transformation been close to the temperature of A1. The role of the second stage, the isothermal one, is also more important in the

first instance than it is in the second. The third, post-isothermal Card 1/2

137-58-3-5846

Conditions for the Formation of Austenite (cont.)

stage plays a more significant role in the second rather than in the first instance. With increasing Cr content it is characteristic for Cr steel to exhibit a slight increase in the inflection temperature and a more pronounced increase in the temperature of A1. In the case of W and Mo steel the positions of the inflection temperature and the temperature of A1 remained unchanged at the concentrations investigated (up to 2 percent Mo and 10 percent W). In the case of Ni steel a sharp reduction in the temperature of A₁ is observed together with an even greater decrease of the inflection temperature. The process of transformation in Cr, W, Mo, and Ni steels heated to an identical temperature may develop differently. An examination of the kinetics of induction heating of alloyed steels makes it possible to determine in advance the heating procedure necessary for the attainment of desired results. Compared with Ni steel, the Cr steel must be heated to a higher temperature in order to effect a complete transformation of the initial phases into austenite. The temperature of tempering must be increased with increasing Cr content and decreased with increasing Ni content. The size of austenite grains must diminish with increasing Cr content and increase with decreasing Ni content.

M. Sh.

Card 2/2

KIDIN IN

137-58-3-5509

Translation from: Referativnyy zhurnal, Metallurgiya, 1958, Nr 3, p146 (USSR)

AUTHOR: Kidin, I. N.

TITLE: High-frequency Induction Tempering of Molybdenum Steel

(Vysokochastotnaya zakalka molibdenovoy stali)

PERIODICAL: Sb. Mosk, in-t stali, 1957, Vol 36, pp 65-74

ABSTRACT: A report on the results of a study concerned with the effect of the conditions of high-frequency induction tempering on the size of

austenite grains (AG) and on the hardness of steel alloyed with 0.2 percent to 2.0 percent of Mo and containing from 0.2 to 1.0 percent of C. A range of tempering temperatures between 880° and 1040° was investigated; it is established that even at such temperatures as 1040° the AG's are smaller in induction tempering than they are at 800°-900° in a standard tempering process, and that the size of AG's diminishes with increasing rates of heating. The greater hardness produced by means of induction tempering in the steels investigated diminishes with increasing Mo content, a fact which is apparently attributable

Card 1/2 to an increased content of residual austenite. Thus the reduction in the size of AG, achieved by means of alloying the steel with

137-58-3-5509

High-frequency Induction Tempering of Molybdenum Steel

Mo, may be intensified by employing high-speed induction heating; this is particularly important in the treatment of products that require improved special properties, such as resistance to breaking, etc.

S. P.

Card 2/2

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ARISTOV, N.P., kand. tekhn. nauk,; BLAGOSKIONSKIY, T.I., kand. khim. nauk,; VESELOVSKIY, V.S., prof., doktor tekhn.nauk,; VLADISLAVLEV, V.S., prof., [deceased]; GOSTENINA, V.M., inzh.; GRINBERG, B.G., kand. tekhn. nauk,; KATTŞ.N.V., kand. tekhn. nauk,; KESTNER, O.Ye., kand. tekhn. nauk,; KIDIN, I.N., prof., doktor tekhn. nauk,; KIRSHENSHTEYN, Ye.L., inzh.; KITAYGORODSKIY, I.I., prof., doktor tekhn. nauk,; KOLOBNEV, I.F., kand. tekhn. nauk,; KRYLOV, V.V., kand. tekhn. nauk,; LAKHTIN, Yu.M., prof., doktor tekhn. nauk,; LEVI, L.I., kand. tekhn. nauk,; LEPETOV, V.A., kand. tekhn. nauk,; LUNEV, A.A., kand. tekhn. nauk,; LUNEV, A.A., kand. tekhn. nauk,; LUNEV, F.A., kand. tekhn. nauk, [deceased]; LOTSMANOV, S.N., kand. tekhn. nauk,; MAURAKH, M.A., kand. tekhn. nauk,; MINKEVICH, A.N., kand. tekhn. nauk,; OCHEIN, A.V., inzh.; POPOV, V.A., kand. tekhn. nauk,; RAKOVSKIY, V.S., kand. tekhn. nauk,; SHESTOPAL, V.M., kand. tekhn. nauk,; ACHERKAN, N.Ş., prof., doktor tekhn. nauk, glavnyy red.; MALOV, A.N., red.; POZDNYAKOV, S.N., red.; ROSTOVIKH, A.Ya., red.; STOLBIN, G.B., red.; CHERNAVSKIY, S.A., red.; KRYLOV, V.I., inzh., red.; KARGANOV, V.G., inzh., red. graficheskikh rabot.; SOKOLOVA, T.F., tekhn. red.

[Netal worker's handbook in five volumes] Spravochnik metallista v piati tomakh. Moskva, Gos. nauchno-tekhn. izd-vo mashinostroit. lit-ry. Vol. 3. Book 1. 1958. 560 p. (MIRA 11:11)

(Metals-Handbooks, manuals, etc.)

SOV/137-58-9-19955

Translation from: Referativnyy zhurnal, Metallurgiya, 1958, Nr 9, p 267 (USSR)

AUTHOR:

Kidin, I.N.

TITLE:

The Effects of Induction-heating Parameters Upon Austenite Grain Size in Chromium Steel (Vliyaniye parametrov induktsionnogo nagreva na velichinu zeren austenita khromistoy stali)

PERIODICAL:

Metallovedeniye i term. obrabotka. Moscow, Metallurgizdat, 1958, pp 50-64

ABSTRACT:

An investigation is made of austenite grain growth in Cr steels containing 0.4, 0.6, 0.8, and 1.0% C and 1, 2.5, and 5% Cr relative to rate of induction heating (10, 50, 100, and 200 degrees/sec) and the temperature to which heating is carried (800, 880, 960, and 1040°C). It is established that the most important factors affecting austenite grain growth are the temperature and rate of heating in the region of austenite formation. Increase in heating rate at identical temperatures reduces grain size, and increase in temperature at identical velocities increases it. An increase in Cr contents to 2.5% (in steels with

Card 1/2

1.0 and 0.8% C) reduces grain growth when heating rate is slow

SOV/137-58-9-19955

The Effects of Induction-heating Parameters (cont.)

(50 degrees/sec). The austenite grain in steel hardened with induction heating is always smaller than the grain of steel hardened in the usual way. The greatest changes in grain size are observed in steels containing 1% Cr.

F.U.

- 1. Induction heating--Metallurgical effects 2. Grains (Metallurgy)--Growth
- 3. Austenite--Temperature factors 4. Chromium steel--Phase studies

Card 2/2

S0V/123-59-23-96998

307/163-58-1-49/53

Translation from: Referativnyy zhurnal. Mashinostroyeniye, 1959, Nr 23, p 115 (USSR)

AUTHOR:

Kidin, J.N.

TITLE:

The Prospects of Development of Theoretical and Technological Investigations in the Field of Induction Heat-Treatment of

PERIODICAL:

Tr. Sektsii metalloved, i term. obrabotki metallov, Tsentr. pravl. Nauchnotekhn. o-va mashinostroit. prom-sti, 1958, Nr 1, pp 3 - 28

ABSTRACT:

The author analyzes the contemporary achievements in the field of induction heat-treatment and the trends in which further theoretical and technological investigations should be carried out. To the theoretical problems which are subject to investigation pertain the kinetic characteristics of induction heating. The rate of heating in the range of phase transformations and the heating temperature should serve as the basic parameters in developing the technology of induction heat-treatment. Based on these parameters, it is possible to plot the diagrams of operation conditions which ensure better qualities in comparison with standard heat-treatment. For a correct application of the conditions of induction heat-treatment every shop or high-

Card 1/2

frequency current section should possess an oscillograph for the recording

APPROVED FOR RELEASE: 06/13/2000 CIA-F CIA-RDP86-00513R000722510017-6"

TITLE:

Radiographic Investigation on the Steel Structure After High Frequency Hardening (Issledovaniye struktury stali posle vysokochastotnoy zakalki metodom radiografii)

PERIODICAL:

Nauchnyye doklady vysshey shkoly Metallurgiya, 1958, Nr : pp 260 - 265 (USSR)

ABSTRACT:

The qualitative and quantitative phase distribution of carbon in the induction expansion of non-eutectoid steels was demonstrated by means of the radiographic method. In all steel samples investigated the heating rate promoted the formation of irregularities in the structures. On the addition of 0,5 % chromium to the steel sample a change in the distribution of carbon as compared to steel sample No. 20 does not occur. With an increase in the chromium content up to 2 % a considerable hampering of the diffusion of carbon in steel occurs A noticeable retardation of the diffusion process occurs in steel samples with 0,5 % tungsten. On the increase of the tungsten content in the steel samples a hampering of the displacement of the diffusion of the carbon atoms from the primary perlite zone

Card : 2

Radiographic Investigation on the Steel Structure After High Frequency Hardening

SOV/163-58-1-49/53

At $V_{\parallel} = 230^{\circ}/\text{sec}$ for the production of carbon concentrations of 0,05% in the medium ferrite ranges of steel with a content of 2% tungsten a heating to 1300°C is necessary.

Molybdenum occurs in the steel samples almost entirely as solid solution and already small additions of molybdenum considerably influence the diffusion of carbon.

In comparing the results with tungsten steels it became evident that in the case of equal amounts of elements to be alloyed and an equal concentration of carbon in the medium ferrite zone the diffusion in molybdenum steels occurs at much higher temperatures than in tungsten steels

With 1 % molybdenum the steel stall has the structure of free ferrite, even when tempered at 1200° C and at V₁₁ = 230°/sec. There are 4 figures, 1 table, and 6 references, 5 of which are Soviet.

Card 2/2

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ASSOCIATION:

Moskovskiy institut stali (Moscow Steel Institute)

SUBMITTED:

October 1, 1957

"APPROVED FOR RELEASE: 06/13/2000 CIA-RDP86-00513R000722510017-6

AUTHORS:

Kidin, I. N., Bashnin, Yu. A.

sov/163-58-2-41/46

TITLE:

The Kinetics of the Isothermal Transformation of Austenite

After Induction Heating (Kinetika izotermicheskogo

prevrashcheniya austenita posleimdukteionnogo nagreva)

PERIODICAL:

Nauchnyye doklady vysshey shkoly. Metallurgiya, 1958, Nr 2,

pp. 227-233 (USSR)

ABSTRACT:

In the induction heating phase transformations occur and it there-

fore is of importance to investigate the kinetics and the

mechanism of the isothermal transformation of austenite. Alloyed steel samples of different composition were used as initial materials with the influence of the alloyed component in the austenite transformation having been taken into account. Comparative isothermal investigations of the austenite transformation were carried out with carbon containing steels in the case of induction and furnace heating. The austenite forming in

induction heating is less stable than that obtained in furnace heating. The decomposition of austenite takes place six times more rapid in the case of induction heating at a temperature

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of 500°C than is the case with austenite obtained by furnace

CIA-RDP86-00513R000722510017-6" APPROVED FOR RELEASE: 06/13/2000

SOV/163-58-2-41/46

The Kinetics and the Isothermal Transformation of Austenite After Induction Heating

heating. The decomposition of austenite obtained by induction heating within the perlite range represents a pure diffusion process. In induction heating austenite occurs in fine grains, which fact accelerates the destruction process. Besides, the austenite obtained in induction heating is irregular and does not have an uniform chemical composition. The most stable austenite is obtained from eutectic steels. When the carbon content in non-eutectic steels is decreased and the carbon content in hypereutectic steels is increased the rate of austenite decomposition increases. Nickel increases the stability of austenite. When the nickel content is increased and the carbon content remains constant the stability of austenite increases. In the case of a constant nickel content and an increased carbon content the stability of sustenite decreases. The decisive factors determining the rate of the decomposition of austenite are first of all the rate of heating within the range of phase transformation; and the temperature of heating. There are 5 figures: 1 table, and 12 references, 12 of which are Soviet.

Card 2/3

The Kinetics and the Isothermal Transformation of Austenite After Induction Heating

ASSOCIATION: Moskovskiy institut stali (Moscow Steel Institute)

SUBMITTED: December 6, 1957

Card 3/3

"APPROVED FOR RELEASE: 06/13/2000 CIA-RDP86-00513R000722510017-6

AUTHOR:

Kidin, I. N.

sov/163-58-3-30/49

TITLE:

The Possibility of the Reversibility of the Martensite Transformation in Steel (Vormorhnost' obnaruzheniya obratimosti martensitnykh prevrashcheniy v stali)

Nauchnyye doklady vyashey shkoly. Metallurgiya, 1958,

Nr 3, op 181 - 188 (USSR)

ABSTRACT:

PERIODICAL:

A method of directly measuring the reversibility of martensite transformations in steel was devised. The transition of the surface layer from the ferromagnetic to the paramagnetic state was made use of. In manganese steels with a carbon content of 0,4% and a manganese content of up to 1% a reversible martensite transformation takes place at a rate of heating of up to 10000° C/sec. In the case of a higher manganese content the reversible martensite transformation takes place on the same conditions and at a lower carbon content. The influence

of the carbon and manganese content on the temperature of the reversible martensite transformation was inves-

Card 1/2

tigated. The results are given in figure 4. Manganese

CIA-RDP86-00513R000722510017-6" APPROVED FOR RELEASE: 06/13/2000

The Possibility of the Reversibility of the Martensite S07/163-58-3-30/49 Transformation in Steel

> steels with 0,22% carbon and 2,4% manganese show no dependence of the temperature of reversible martensite transformation on the rate of heating. At a rate of heating of 2500° C/sec. - 15000° C/sec. the reversible martensite transformation takes place within the temperature range of $660-670^{\circ}$ C. With the same carbon content and the same alloyed elements the reversible martensite transformation in chromite steels is higher than with manganese steels. In caromite steels with a chremium content of 5-6% the transformation temperature is by 150-160° C higher. There are 5 figures, 1 table, and 10 references, all of which are Soviet.

ASSOCIATION: Moskevskiy institut stali (Moscow Steel Institute)

SUBMITTED:

May 8, 1958

Card 2/2

"APPROVED FOR RELEASE: 06/13/2000 CIA-RDP86-00513R000722510017-6

18(7)

AUTHOR: -Kiding I. R.

SOV/163-58-4-39/47

TITLE:

Influence of the Rate of Heating on the Fine Structure of Nickel Iron (Vliyaniye skorosti nagreva na tonkuyu strukturu

nikelevogo zheleza)

PERIODICAL:

Nauchnyye doklady vysshey shkoly. Metallurgiya, 1958, Nr 4,

pp 225-228 (USSR)

ABSTRACT:

The influence of the rate of heating on the fine structure of nickel iron was investigated. Engineer R. M. Paretskaya (a woman) took part in the experiments. The alloy was prepared from technically pure iron and metallic nickel in a 10-kg induction

furnace. The chemical composition of the alloy was: 0.05% C,

C.39% Mn, O.08% Si, 7.50% Ni, O.034% S, O.017% P. The analysis of the data obtained shows the following: the rate of heating has a certain influence on the magnitude of the observed ranges of nickel iron. An increase in the quenching temperature causes an increase in mosaic blocks, but the degree of reduction of this magnitude is virtually independent of the heating temperature for quenching, at an increase in the rate of

heating up to 50 and 15000/sec in nickel iron. An essential increase in the tensions of second type is only observed at a

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"APPROVED FOR RELEASE: 06/13/2000 CIA-RDP86-00513R000722510017-6

Influence of the Rate of Heating on the Fine Structure of Nickel Iron

SOV/163-58-4-39/47

very high increase in the rate of heating - up to 15000/sec. At increase in hardness at an acceleration of heating corresponds to the character of the change of magnitude for otherent ranges. In nickel iron, the rate of heating has an influence on the elements of fine structure and the hardness in the same direction as in chrome iron. In addition, the hypothesis on the formation of austenite nuclei on the tundardes of the mosaic blocks of the initial ferrite at a high rate of heating was again proved in the present investigation. The results of the investigation also confirm the possibility of obtaining finer mosaic blocks. There are 1 figure, 1 table, and 6 Soviet references.

ASSOCIATION: Moskcyskiy institut stali (Moscow Steel Institute)

SUBMITTED: May 29, 1958

Card 2/2

129-58-7-2/17

Kidin, I. N.; Doctor of Technical Sciences, Professor AUTHORS:

and Bashnin, Yu. A., Engineer

Kinetics of Isothermal Transformation of Austenite of Carbon Steel During Induction Heating (Kinetika TITLE:

izotermicheskogo prevrashcheniya austenita uglerodistoy

stali pri induktsionnom nagreve)

PERIODICAL: Metallovedeniye i Obrabotka Metallov, 1958 Nr 7

pp 10-15 (USSR)

In earlier work the authors of this paper (Refs 3 and 4) ABSTRACT:

and other authors (Refs. 5 and 6) have shown that

austenite forming during induction heating is characterised by a non-uniform chemical composition, the degree of which depends on the head regime and on the nature of the heated steel. In this work the authors investigate the kinetics and the mechanism of isothermal decomposition of the austenite as a function of the composition of the

steel and the austenisation regime. The chemical

compositions of the selected steels are entered in Table 1, p.ll. The kinetics of the isothermal decomposition

were studied by the magnetometric method. For comparison and for better elucidation of the specific features of decomposition of the austenite obtained as a result of

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129-58-7-2/17 Kinetics of Isothermal Transformation of Austenite of Carbon Steel During Induction Heating

induction heating the austenite decomposition was are studied after ordinary heating in the furnace with heating regimes as enumerated in Table 2, p.ll. Isothermal transformation diagrams as well as the obtained kinetic curves of austenite decomposition are given. On the basis of the obtained results the following conclusions are arrived at:

1) For the investigated grades of steel the austenite has a lower stability in the case of induction heating than in the case of ordinary heating due to the larger non-uniformity of the carbon distribution and the fact that the austenite grains are finer;
2) The kinetics of decomposition of the austenite which

2) The kinetics of decomposition of the austenite which forms during induction heating is similar to the kinetics pertaining to ordinary heating for the pearlitic temperature range. There is no justification for assuming that the mechanism differs from that of decomposition of austenite obtained in the case of slow heating;

Card 2/3 3) Transformation of the austenite obtained during

the 129-58-7-2/17 Kinetics of Isothermal Transformation of Austenite of Carbon Steel During Induction Heating

induction heating in the intermediate range begins according to the martensitic kinetics with subsequent superposition of the diffusion process of carbon redistribution in the austenite. This conclusion can be made by considering the transformation after induction heating as being of a two-stage nature;

4) A decisive factor determining the characteristic of decomposition of austenite obtained during induction heating is the regime of austenisation: the speed of heating and the range of phase transformations and the heating temperature, i.e. the magnitudes determining the uniformity of the composition of the austenite and its grain size.

There are 3 figures, 2 tables and 9 references.

8 of which are Soviet, 1 English.

ASSOCIATION: Moskovskiy institut stali (Moscow Steel Institute)

Card 3/3

SOV/129-58-9-1/16

Kidin, I. N. Doctor of Technical Science, Professor; Astaf yeva, Ye. V. and Marshalkin, A. N., Engineers AUTHORS:

Features of the Process of Tempering After High TITIE:

Frequency Hardening (Osobennosti protsessa otpuska posle

vysokochastotnoy zakalki)

PERIODICAL: Metallovedeniye i Obrabotka Metallov, 1958, Nr 9,

pp 2-12 + 1 plate (USSR)

ABSTRACT: "Self tempering", the duration of which is a few seconds, is in many cases convenient and economical (Refs 1 and 2).

However, this type of heat treatment has not been used adequately due to non-availability of the necessary automatic control and metering apparatus. Of great interest are the results relating to combination of electric tempering with electric hardening (Refs 3-5). An important condition of electric tempering is that uniform heating should be achieved, to the desired depth, without overheating of the surface. In earlier work of

the authors (Refs 6-10) it was found that

if the speed of heating for hardening is high, the state of the austenite is characterised by a considerable

Card 1/8 non-uniformity in the carbon content as compared to

sov/129-58-9-1/16 Features of the Process of Tempering After High Frequency Herdening

austenite formed during ordinary slow heating. As a result of this non-uniformity, the austenite to martensite transformation during the cooling will take place within a wider temperature range; the micro-volumes of the austenite which are most saturated with carbon become transformed into martensite at lower temperatures and later than the micro-volumes which are poor in carbon and for which the martensitic point is located at a more elevated temperature. The microvolumes of the martensite forming at a higher temperature may decompose during the further cooling of the hardening process forming martensite of a lower tetragonality and a finely dispersed carbide phase. A similar phenomenon for tempering after ordinary hardening was investigated in detail by Kurdyumov, G. V. and Oslon, N. (Ref 10) by In this paper the authors investigate X-ray methods. the changes in the structural state and the mechanical properties of a number of engineering and carbon tool steels during ordinary tempering in conjunction with regimes of high frequency hardening and the features of the Card 2/8 obtained structure. In the case of rapid induction heating

797/129-9-1-9-1/16 Process of Semering After High Frequency Hurdening

of steel prior to hardening, a concentration non-uniformity can be created in the micro-volumes. Study of this nonuniformity by radiography methods has enabled astablishing the fact that the distribution of the cerbor at the end of the induction heating may differ, depending on the heating regime and the character of the initial structure. Micro-structures and micro-radiograms of Steel 20 hardened from 1100°C with various heating speed are reproduced in Fig.1 (plate). The structure is relatively uniform in the case of slow heating, whilst with increasing heating speeds the non-uniformity in the carbon distribution becomes much more prenounced. This was also confirmed The features of decomposition Juring by X-ray studies. tempering of the non-uniform martensite were also studied; the graph Fig. 3 indicates the curves of the charges of the (110) lines after tempering of specimens of the Secol U? and, by comparing the appropriate curves, it can be seen that an increase in the heating speed for heating to the same temperature, e.g. 960°C, results in an increase in the width of the line and consequently also in an increase Card 3/8 in the non-uniformity. In Fig. 4 the changes are graphed

BOV/129-58-9-1/16

Features of the Process of Tempering After High Frequency Hardening

of the maximum carbon concentration during temperang of Steel 40 which prior to hardening was heated with a speed of 130 C/sec from 920 and 960 C respectively. The influence of low temperature tempering on the merbranical properties after high frequency hardening was lovestigated by the continuous-successive method on the Sleeks 40 and 35 Kh; for the impact tests, specimens of 11,33 and die. were chosen in accordance with the suggestion of I. V. Kudryavtsev (Ref 15). 100 mm leng specimens were hardened using as a current source a subo oscillator, the heating speeds in the regions of phase transformations were 50, 100, 200 and 400 C/sec for the temperatures 900, 1000 and 1100 C. The tempering was effected at 120, 150, 180 and 200 C for heating durations of 15, 30 and 60 minutes. From the tempered specimens the centre part of a length of 55 mm was cut out by the anodomechanical method and in this a 0.5 mm nation with a recommechanical method and in this a 0.5 mm notch with a recens angle of 60 was made. Specimens which have been hardened right through have been tested on an impact machine using an impact of 10 kgm. The influence of the high

Card 4/8 frequency hardening on the impact strength after tempering

Features of the Process of Tempering After High Frequency Hardshin.

is quite considerable as can be seen from the prophs, Fig.5; in the case of Steel 40 a heating speed of 50 C/sec will ensure an impact strength equal to the impact strength obtained after ordinary hardening god tempering only if the tempering is effected at 900°C. Increase of the hardening temperature to 1000 and 1100°C leads to a considerable decrease of the impact strength. However, an increase in the heating speed prior to hardening to 200°C, and particularly to 400°C, followed by tempering will ensure a considerable improvement of the combination of the toughness and hardness. The highest impact strength was obtained in the case of tempering at 200°C for one hour after hardening from a temperature of 1000°C using a heating speed of 400°C/sec. By using this regime an impact strength is obtained which is almost double that obtained after ordinary hardening followed by equal tempering. In Fig.6 the change of the impact strength after hardening followed by low temperature tempering is graphed for the Steel 40 hardened from 920°C after heating at a rate of 170°C/sec. The breeking Card 5/8 strength was measured of ctandard notched arecine of

Features of the Process of Tempering After High Projector Features of the Process of Tempering After High Projector Features of the Process of Tempering After High Projector Features of the Process of Tempering After High Projector Features of the Process of Tempering After High Projector Features of the Process of Tempering After High Process

40KhN steel which were bested prior to bardening with a current of 2.5 kc/sec, a heating speed of 20°C/sec to 970°C and, after hardening, they were tempered for one hour at 120, 150 and 180°C respectively. For comparison the breaking strength was also accounted of opecimens after ordinary hardening and low temperature tempering. It can be seen from Fig.7 that the hardening strength for induction hardening as well as ordinary hardening increases with increasing temperature of the low temperature tempering. Specimens hardened from 970°C after heating at a rate of 20°C/sec showed an increase in the breaking strength from 8 to 9.8 tons after tempering at 120°C and to 11.3 tons after tempering at 180°C. The changes in the mechanical properties were also investigated for medium and high temperature tempering for the Steels 40KhN and 40 KhG. Hardening from 1000°C followed by tempering ensures for the steel 40KhN the same properties as ordinary hardening followed by tempering. However, hardening from 900°C with the same speed of heating and subsequent tempering produces an optimum combination of the properties, namely, a higher

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Features of the Process of Tempering After High Frequency Hardening

impact strength and hardness than after ordinary hardening and tempering. In the case of heating prior to hardening with a speed of 400°C/sec advantages compared to ordinary hardening are observed in the case of hardening from 1000 and 1100 C; the impact strength will be lower in the case of hardening from 1200°C. The heating speed of 100°C/sec is inadvisable since for the chosen temperatures of hardening and subsequent tempering the impact strength will be lower than for ordinary hardening. For tempering temperatures exceeding 350°C the increase in hardness due to high frequency hardening does not remain conserved for the Steels 40KhK and 40KhG. At higher tempering temperatures (up to 600°C) the hardness of high frequency hardened steel may in some cases be lower than of the same steel after conventional hardening which is obviously due to a difference in the kinetics of the processes of coagulation in steel hardened after induction heating. High frequency hardening does not suppress type I and type II temper brittleness. These are observed at the same tempering temperatures as for conventionally hardened steel.

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sov/129-58-9-1/16

Features of the Process of Tempering After High Frequency Hardening

However, the impact strength at the temper brittleness temperatures is considerably higher for steels which were high frequency hardened under optimum heating regimes than for steels which were hardened by standard methods of heating. The here given experimental data indicate that there is a relation between the regime of high frequency hardening and the subsequent tempering, i.e. between the character of the distribution of carbon and the alloying elements after hardening and their redistribution after tempering, which has a considerable influence on the changes of the mechanical properties of hardened and tempered steel.

There are 7 figures and 16 references, 15 of which are Soviet, 1 English.

ASSOCIATION: Moskovskiy institut stali (Moscow Steel Institute)

- 1. Steel--Heat treatment 2. Tool steel--Heat treatment
- 3. Steel--Properties 4. Steel--Transformations 5. High frequency heating--Applications

Card 8/8

BARDIN, I.P., akademik; DYMOV, A.M., prof., doktor khim.nauk; DIKUSHIN, V.I.; akademik; TSHLIKOV, A.I.; OTLEV, I.A., inzh. (g. Khimki, Moskovskoy oblasti).; DEM'YANYUK, F.S., prof., doktor tekhn.nauk; RYEKIN, A.P., prof., doktor tekhn.nauk; YAKUSHEV, A.I., prof., dokt. tekhn.nauk; KIDIN, I.N., prof. doktor tekhn.nauk; KOROTKOV, V.P., dots., kand. tekhn.nauk; SHUKHGAL'TER, L.Ya., dots., kand.tekhn.nauk; KUKIN, G.N., prof., doktor tekhn.nauk.

Every specialist should know the principles of of standardization.
Standartizatsiia 22 no.4:34-40 Jl-Ag '58. (MIRA 11:10)

1.Chlen-korrespondent AN SSSR (for TSelikov). 2.Predsedatel' tekhniko-ekonomicheskogo soveta Mosobisovnarkhoza (for Rybkin). 3.Direktor

Moskovskogo instituta stali imeni I.V. Stalina (for Kidin). 4.Direktor

Moskovskogo vechernégo mashinostroitel'nogo instituta (for Korotkov).

(Standardization--Study and teaching)

SOV/137-58-11-22972

Translation from: Referativnyy zhurnal. Metallurgiya, 1958, Nr 11, p 163 (USSR)

AUTHOR: Kidin, I. N.

TITLE: Characteristics of the Passing of Carbon Into Solid Solution Upon

Induction Heating of Chromium Steel (Usloviya perekhoda ugleroda v tverdyy rastvor pri induktsionnom nagreve khromistoy stali)

PERIODICAL: Sb. Mosk. in-t stali, 1958, Vol 38, pp 405-419

ABSTRACT: The kinetics of the passing of Carbon (C) into solid solution upon

induction heating of specimens of Cr steel containing (in%): C 0.6 0.8, and 1.0 and Cr 1.0, 2.5, 5.0, and 10.0, were investigated by the X-ray diffraction method. The heating was carried out at a rate of 40, 75, 130, and 200°C/sec to 880, 960, and 1040°C temperatures. It is established that the passing of C into solid solution is more complete in steel with 1.0% Cr than in steel with from 5 to 10% Cr; in the latter a major portion of C remains in the carbides. The retardation in the dissolution of carbides occurring upon an increase in Cr content is explained by the fact that steels with 1.0% Cr contain carbides of the cementite type, whereas the major portion of carbides

Card 1/2 in steels with 5% Cr and all the carbides in steels with 10% Cr

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SOV/137-58-11-22972 Characteristics of the Passing of Carbon Into Solid Solution (cont.)

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